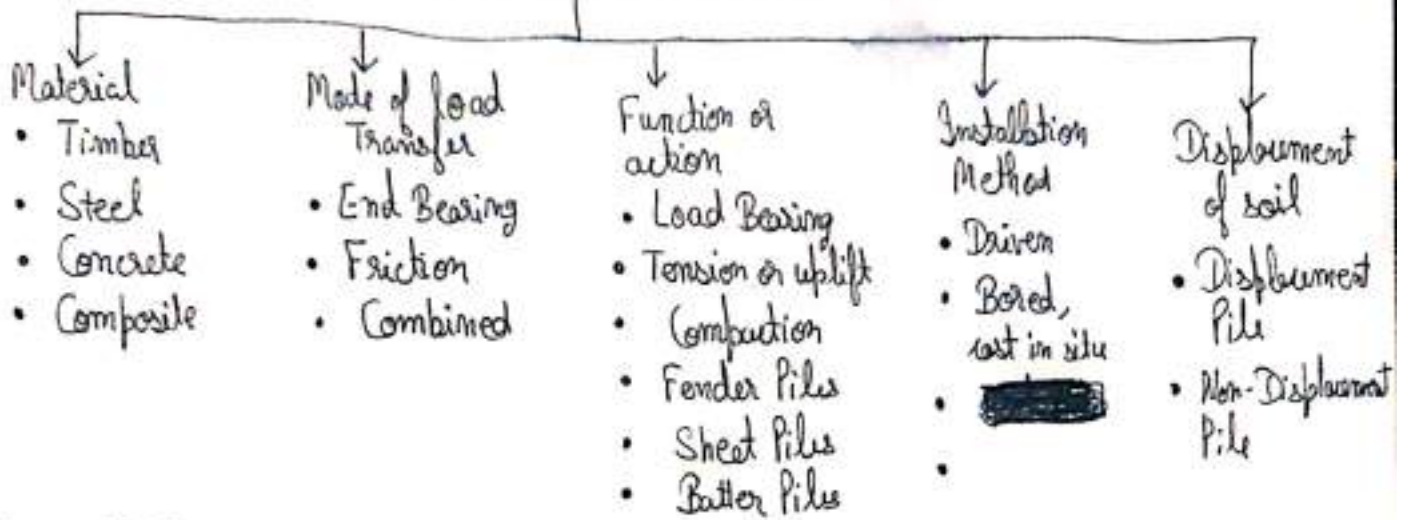


PILE FOUNDATION

Pile: Small diameter shaft is driven or bored into ground.

Piers & Wells: Large diameter shaft is constructed by excavation and then it is sunk to required depth.

Classification of Pile

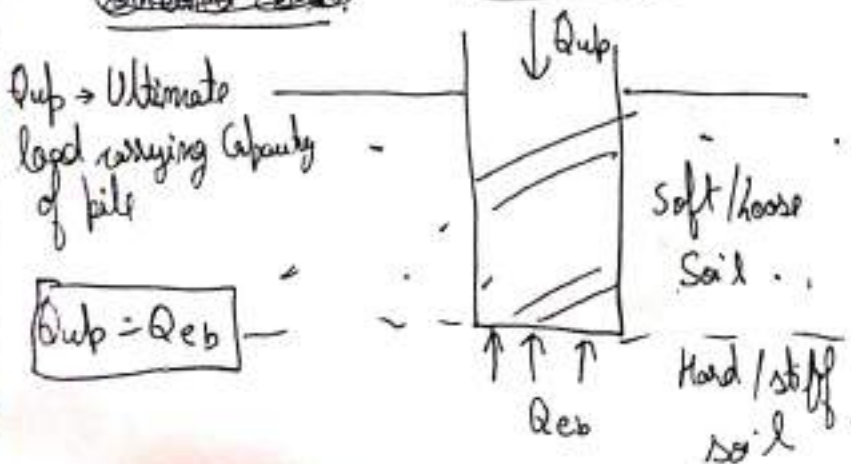


End Bearing Piles: Develop most of their load bearing capacity at the toe of the pile, taking support on strong soil or rock.
Used in stiff clay or dense sand. (at base) → Hard soil is at base

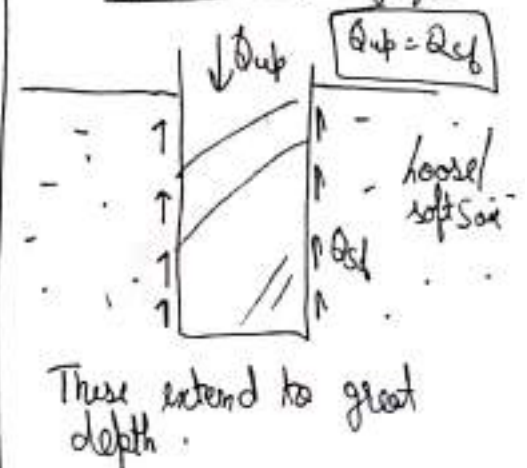
Friction Pile: It is a type of pile that utilizes the frictional resistance force between the pile surface and adjacent soil to transfer the superstructure load.

Used in Soft Soil & Clay.

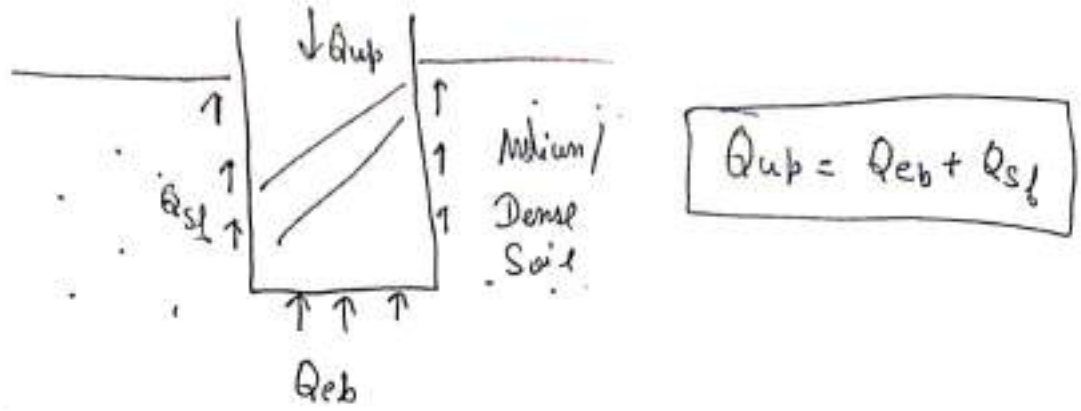
~~Combined Pile~~ End Bearing:



Friction Pile / Hanging:

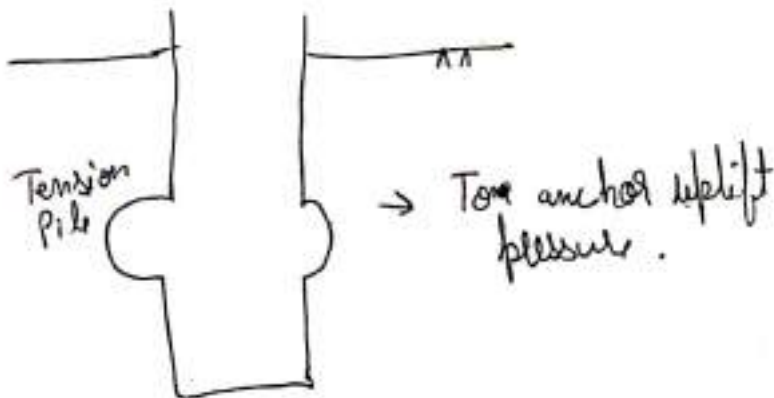


Combined Pile: If Piles are driven in medium to stiff soil, then load carrying capacity is due to combined effect of end bearing action & skin friction both.

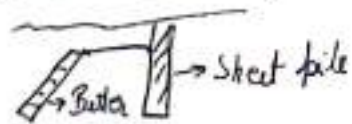


On Basis of function or action:

- 1) Load Bearing Pile: It transmits the load of building through a layer of soil to stronger layer of soil.
- 2) Compaction Pile: These are driven in loose sand in order to increase its density & bearing capacity.
 - ↳ to compact a surface to inc. bearing capacity
 - It is drawn near the seas or river to avoid the process of liquefaction.
- 3) Tension / Uplift Pile: These type of piles are used to anchor the structure subjected to uplift pressure caused by swelling of soil such as in black soil.



- 4) Fender Pile: used to anchor the structure subjected to tidal wave caused by seismic activities
 → Used in water front structures.
- 5) Batter Pile: These piles are driven in inclined ~~direction~~ direction to prevent horizontal ~~force~~ thrust.
 → Used in water front structures
- 6) Sheet piles: It is used to retain the earth mass & also used below the hydraulic structures to minimize piping failure.



Installation Mtd:

- 1) Driven pile: Pile driver is a device used to drive piles into soil.
- 2) Bored piles: are piles where the removal of soil forms hole for a reinforced concrete pile which is poured in situ.

On Basis of Displacement of Soil.

- ① Displacement Piles: The piles which displace the soil and causes disturbance while driving are called displacement pile.
- ② Non-displacement piles: When it does not displace or does not disturb the ~~so~~ adjacent soil it is called non-displacement piles.

Ultimate load carrying capacity of pile: (Q_{up})

- It is the total load which can be applied on pile without shear failure.
- Ultimate load carrying capacity is sum of end bearing resistance and surface friction/skin friction $Q_{up} = Q_{cb} + Q_{sf}$

Allowable or Safe load of pile: (Q_{ap} / Q_{safe})

- It is the max safe load which can be allowed on the pile without risk of shear failure.

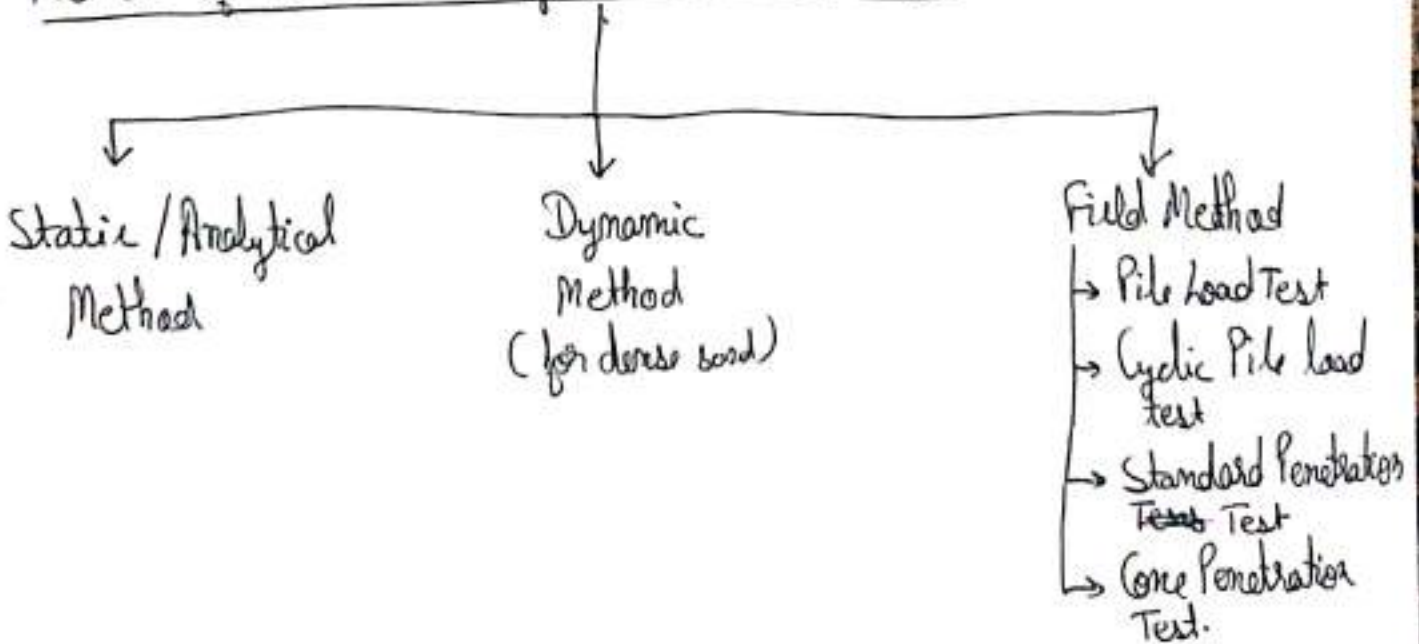
$$Q_{ap} / Q_{safe} = \frac{Q_{up}}{F.O.S}$$

Q_{cb} → end bearing load
 Q_{sf} → surface friction load / skin friction load

$$Q_{safe} = \frac{Q_{cb} + Q_{sf}}{F.O.S}$$

F.O.S = 2.5 to 3

Method of determination of Pile load Capacity:



Note: Cyclic Pile load test gives end bearing resistance & skin friction resistance separately.

D) Static / Analytical Method:

$$Q_{up} = Q_{eb} + Q_{sf}$$

$$Q_{eb} = q_b \cdot A_b$$

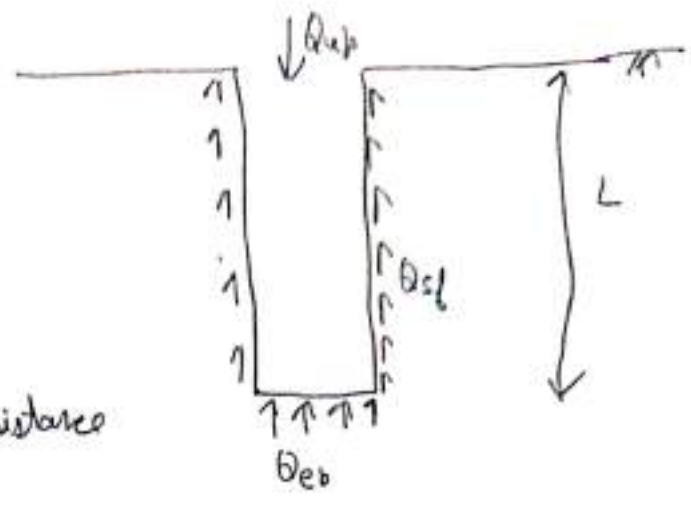
$$Q_{sf} = q_s \cdot A_s$$

q_b → ~~unit~~ ^{end} bearing resistance

A_b → Area of base

q_s → Unit skin friction resistance

A_s → Surface area of pile



	Circular	Square
A_b (base area)	$\frac{\pi}{4} D^2$	B^2
A_s (skin surface area)	$\pi D L$	$4 B L$

$$Q_{up} = q_b A_b + q_s A_s$$

Case 1: For Clay (C-soil):

q_b = End Bearing resistance
 = Ultimate bearing capacity at base

As per Meyerhoff: $q_b = 9C$ → for clay soil
 C → Unit Cohesion

q_s = side resistance

$$q_s = \alpha \bar{c} \quad \bar{c} = \text{avg cohesion along length of pile}$$

α = adhesion factor b/w pile & soil.

- $\alpha = (0.6 \text{ to } 0.9) \rightarrow$ for soft clay
- $\alpha = (0.4 \text{ to } 0.6) \rightarrow$ Medium clay
- $\alpha = (0.2 \text{ to } 0.4) \rightarrow$ Stiff clay

Ultimate load Carrying Capacity of Pile in Clay:

$$Q_{up} = Q_{eb} + Q_{sf}$$

$$Q_{up} = q_b A_b + q_s A_s$$

$$Q_{up} = q_c A_b + \alpha \bar{c} A_s$$

Note: For very long pile ($L \geq 25m$) the above Mtd is very conservative. For such piles, unit skin friction also depends upon effective overburden pressure.

\therefore Avg. unit friction can be represented by:

$$q_s = \lambda (\bar{\sigma}_v + 2\bar{c})$$

$\lambda =$ friction capacity factor
 $\bar{\sigma}_v =$ Mean eff. stress

$$Q_{up} = q_c A_b + \lambda (\bar{\sigma}_v + 2\bar{c}) A_s$$

Case 2: For Sand (For ϕ soil)

As per Meyerhoff $\Rightarrow q_u = c + \gamma D_f N_q + 0.5 B \gamma N_\gamma$

$\ll \gamma D_f N_q \gg 0.5 B \gamma N_\gamma$
 \hookrightarrow as $B \ll D_f$

$\therefore q_u = \gamma D_f N_q$ where $D_f =$ Depth of footing = L

$$q_u = \gamma L N_q$$

$q_b =$ end bearing resistance
 $=$ ultimate bearing capacity at base

$$q_b = \gamma L N_q$$

$N_q =$ Meyerhoff. Bearing Capacity factor

q_s = skin friction resistance (for sand)

$$q_s = \mu (\text{avg. earth press.})$$

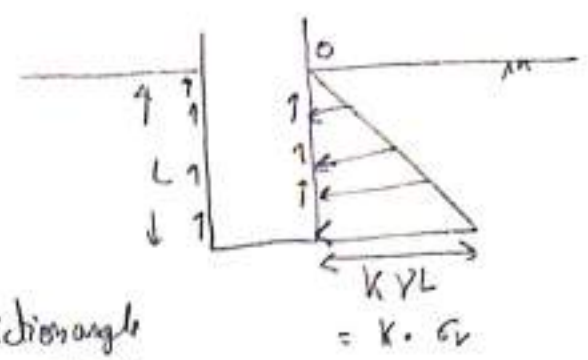
$$= \mu \left(\frac{0 + K \sigma_v}{2} \right)$$

$$= \frac{\mu K \cdot \gamma L}{2}$$

$\sigma_v = \gamma L$

$\mu = \text{friction angle}$

$\mu = \tan \delta$



$q_s = \left(\frac{K \gamma L}{2} \right) \tan \delta$

$K = \text{earth press. coeff.}$

$L = \text{Length of pile}$

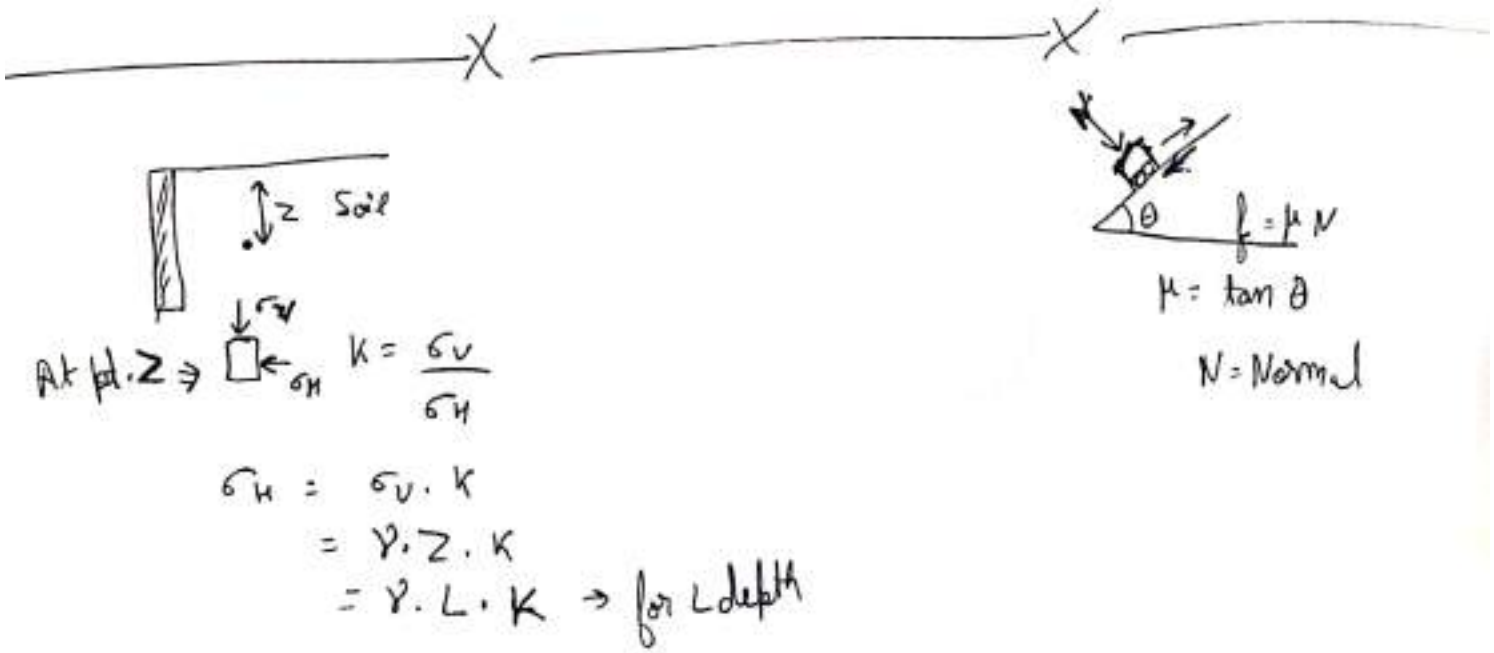
$\delta = \text{friction angle b/w pile \& soil}$

$q_s = \frac{1}{2} K \cdot \gamma L \tan \delta$

Ultimate load capacity for sand:

$Q_{up} = q_b A_b + q_s A_s$

$Q_{up} = (\gamma L N_q) \cdot A_b + \left(\frac{1}{2} K \gamma L \tan \delta \right) A_s$ **



2) Dynamic Method:

- This analysis is based on the assumption that the dynamic resistance to drive the pile is equal to the ultimate load capacity using static method.
- In this the ~~kinetic~~ kinetic energy / Potential energy of hammer is equal to work done by pile.

Energy Impacted = $W \times H$

a) Engineering News Formula:

$Q_{up} = \frac{WH}{S+C}$

$Q_{allowable} = \frac{WH}{F.O.S(S+C)}$ * (in kN) → For drop hammer or single acting steam hammer

W = ~~load~~ Wt. of hammer in kN

H = Ht. of free fall of hammer in cm

S = Settlement per blow of hammer in cm

Settlement is taken as avg. value of last 5 blow

~~C~~ for drop hammer

or it is equal to last 20 blows of steam hammer

C = Empirical factor

= 2.5 cm → For drop Hammer

= 0.25 cm for single acting steam hammer

$F.O.S = 6$

(b) Hiley's Formula:

$$Q_{up} = \eta_h \cdot \eta_b \left(\frac{WH}{S + \frac{C}{2}} \right)$$

Safe load carrying Capacity of soil:

$$Q_{safe} / Q_{ap} = \frac{Q_{up}}{3} = \frac{Q_{ub}}{3}$$

$$F.O.S = 3$$

W = Wt. of hammer in kN

H = Height of free fall in cm

S = Final set per blow in cm

C = Total elastic compression per blow
i.e of soil + ~~pile~~ pile

η_h = efficiency of hammer

$\eta_h = 1$ → drop hammer

$\eta_h = 0.75$ to 0.85 → Single acting steam hammer

$\eta_h = 0.7$ to 0.8 → double acting steam hammer

η_b = efficiency of hammer blow

2. Determine the safe load for pile of 30 cm dia driven into a medium dense sand ($\gamma = 21 \text{ kN/m}^3$, $k = 1.0$, $\tan \delta = 0.70$)
 Depth of pile = 3.6 m. Take F.O.S = 2.5 ; $N_q = 66$

\Rightarrow Vertical press = $3.6 \times 21 = 75.6 \text{ kN/m}^2$

$$Q_{up} = (\gamma L N_q) A_b + \left(\frac{1}{2} k \gamma L \tan \delta\right) A_s$$

$$= 21 \times 3.6 \times 66 \times \frac{\pi}{4} \times (0.3)^2 + \left(\frac{1}{2} \times 1 \times 21 \times 3.6 \times 0.70\right) \pi \times 0.3 \times 3.6$$

$$Q_{up} = 1282.52 + 87.77$$

$$= 1372.296 \text{ kN}$$

$$Q_a = \frac{1372.296}{2.5} = \underline{\underline{548.92 \text{ kN}}}$$

6. A 30 cm dia concrete pile is driven into homogeneous consolidated clay deposit ($C_u = 40 \text{ kN/m}^2$, $\alpha = 0.7$).
 If the embedded length is 10 m, estimate safe load (F.O.S = 2.5)

~~Answer~~

\Rightarrow $Q_u = q_c A_b + \alpha \bar{c} A_s$

$$= (9 \times 40) \frac{\pi}{4} (0.3)^2 + 0.7 \times 40 (\pi \times 0.3) 10$$

$$= 289.2 \text{ kN}$$

$$Q_a = \frac{Q_u}{2.5} = \frac{289.2}{2.5} = \underline{\underline{115.7 \text{ kN}}}$$