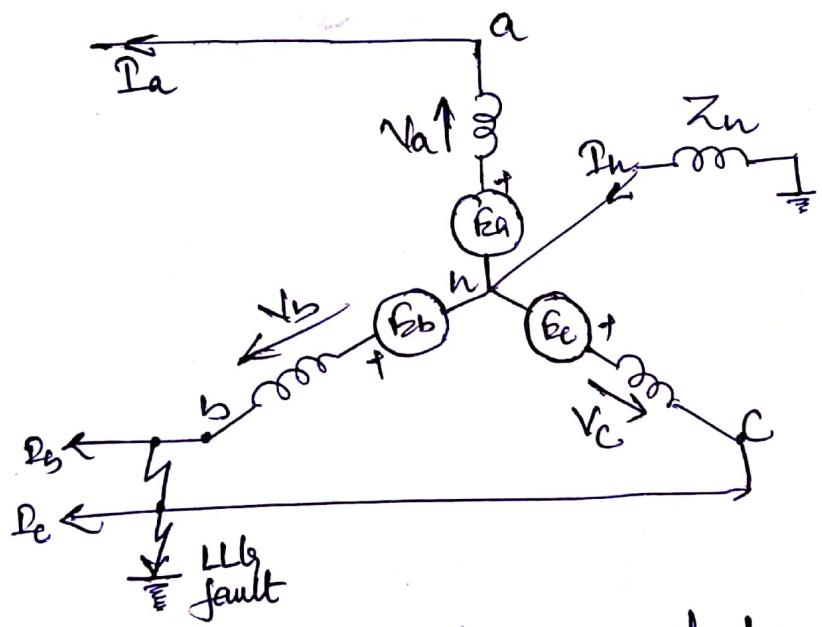


Double Line-to-Ground (LLG) fault



Consider a double-line to ground fault at the terminal of a unloaded generator, whose neutral is grounded through a reactance, between phase 'b' and 'c' as shown in fig.

Consider fault conditions —

$$I_a = 0 \quad \& \quad V_b = V_c = 0 \quad \longrightarrow ⑯$$

Symmetrical component of voltage with $V_b = V_c = 0$

$$V_{ao} = \frac{1}{3} (V_a + V_b + V_c) \\ = V_a/3$$

~~$$V_{ai} = \frac{1}{3} (V_a + \alpha V_b + \alpha^2 V_c)$$~~

$$V_{ai} = \frac{1}{3} (V_a + \alpha V_b + \alpha^2 V_c) \\ = V_a/3$$

$$V_{a2} = \frac{1}{3} (V_a + \alpha^2 V_b + \alpha V_c) \\ = V_a/3$$

Hence

$$V_{ao} = V_{ai} = V_{a2} = V_a/3 \quad \longrightarrow ⑯$$

Using this relation of voltage and substituting
in the sequence network eqn. ②

$$V_{ao} = V_{ai}$$

$$-I_{ao}Z_0 = E_a - V_{ai}Z_1$$

$$I_{ao} = \frac{-(E_a - I_{ai}Z_1)}{Z_0} \quad \longrightarrow ⑰$$

Similarly

$$V_{ao} = V_{ai}$$

$$-I_{a2}Z_2 = E_a - I_{ai}Z_1$$

$$I_{a2} = -\frac{(E_a - I_{a1}Z_1)}{Z_2} \quad \xrightarrow{\text{Eqn. 18}} \quad 18$$

Now from eqn. 15

$$I_a = I_{a1} + I_{a2} + I_{ao} = 0$$

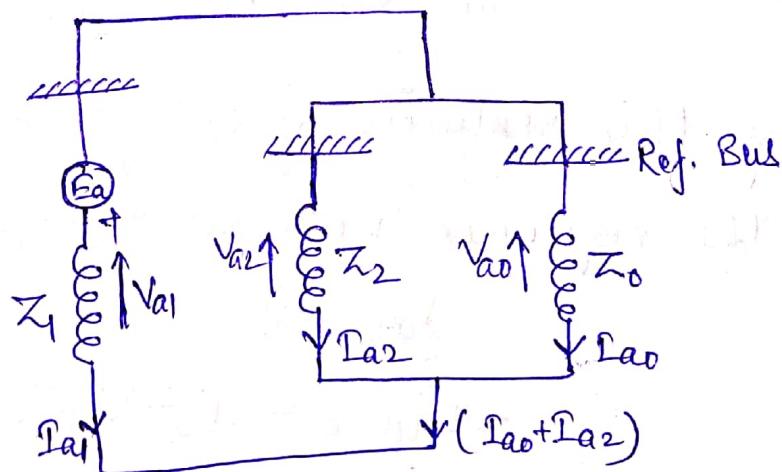
Now substitute the value of I_{ao} & I_{a2} from eqn. 17 & 18

$$I_{a1} - \frac{(E_a - I_{a1}Z_1)}{Z_2} - \frac{(E_a - I_{a1}Z_2)}{Z_0} = 0$$

After rearranging the terms —

$$I_{a1} = \frac{E_a}{Z_1 + \frac{Z_0 Z_2}{Z_0 + Z_2}}$$

19



Eqn. 19 implies that, to simulate the LLg fault, the three sequence networks are connected such that the positive N/W is connected in series with the parallel combination of the negative and zero sequence networks as shown in above figure.

LL fault with impedance Z_f

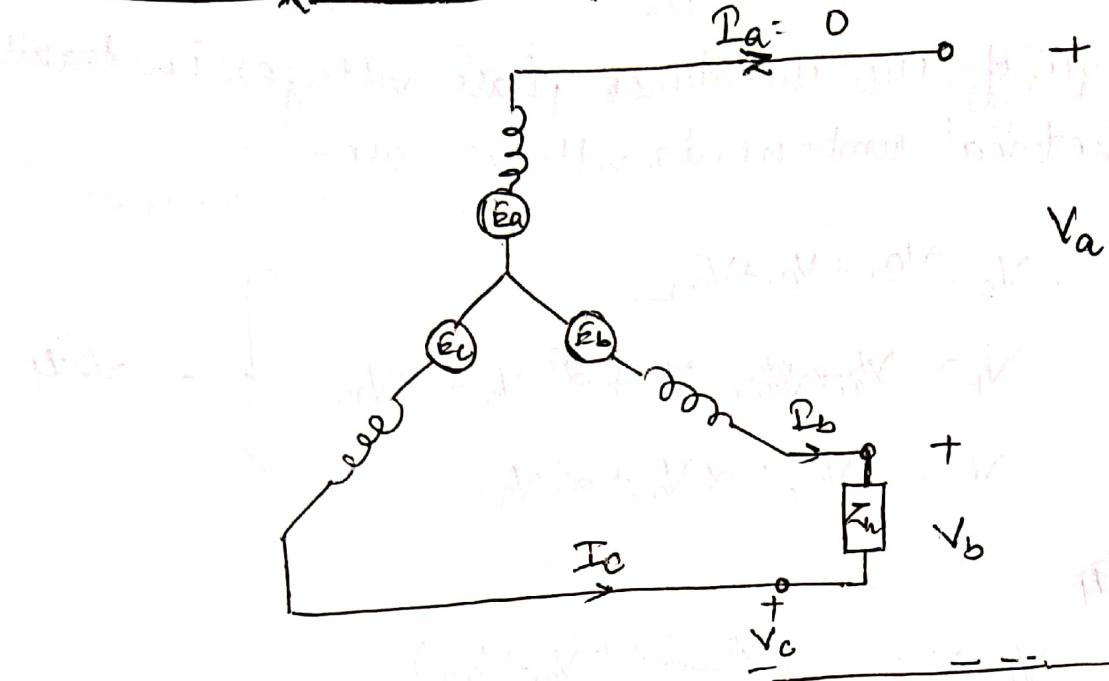


Figure shows a 3 ϕ generator with fault through an impedance Z_f between phases b and c. Assuming the generator is initially on no load, the boundary conditions at the fault point are —

$$V_b - V_c = Z_f I_b$$

$$I_b + I_c = 0 \text{ or } I_b = -I_c$$

$$I_a = 0$$

Substituting for $I_a = 0$, and $I_c = -I_b$, the symmetrical components of currents from —

$$\begin{bmatrix} I_{a0} \\ I_{a1} \\ I_{a2} \end{bmatrix} = \frac{1}{3} \begin{bmatrix} 1 & 1 & 1 \\ 1 & \alpha & \alpha^2 \\ 1 & \alpha^2 & \alpha \end{bmatrix} \begin{bmatrix} 0 \\ I_b \\ -I_b \end{bmatrix} \rightarrow (21)$$

After solving the above eqn.

$$I_{a0} = 0$$

$$I_{a1} = \frac{1}{3} (\alpha - \alpha^2) I_b$$

$$I_{a2} = \frac{1}{3} (\alpha^2 - \alpha) I_b$$

$\rightarrow (22)$

from eqn. no. (22)

$$I_{a_1} = -I_{a_2} \longrightarrow (23)$$

From the eqn. of the unbalance phase voltages in terms of the symmetrical components voltages are —

$$\left. \begin{aligned} V_a &= V_{a_0} + V_{a_1} + V_{a_2} \\ V_b &= V_{a_0} + \alpha^2 V_{a_1} + \alpha V_{a_2} \\ V_c &= V_{a_0} + \alpha V_{a_1} + \alpha^2 V_{a_2} \end{aligned} \right\} \longrightarrow (24)$$

from eqn. (24)

$$\begin{aligned} V_b - V_c &= (\alpha^2 - \alpha)(V_{a_1} - V_{a_2}) \\ &= Z_n I_b \end{aligned}$$

$$(\alpha^2 - \alpha)(V_{a_1} - V_{a_2}) = Z_n I_b \longrightarrow (25)$$

from eqn. (2)

$$(\alpha^2 - \alpha) [(E_a - Z_1 I_{a_1}) - (-Z_2 I_{a_2})] = Z_n I_b$$

$$(\alpha^2 - \alpha) [E_a - Z_1 I_{a_1} + Z_2 I_{a_2}] = Z_n I_b$$

from eqn. (23)

$$(\alpha^2 - \alpha) [E_a - (Z_1 + Z_2) I_{a_1}] = Z_n I_b$$

from eqn. (22)

$$E_a - (Z_1 + Z_2) I_{a_1} = \frac{3 Z_n I_b}{(\alpha - \alpha^2)(\alpha^2 - \alpha)} \longrightarrow (26)$$

After solution the value of $(\alpha - \alpha^2)(\alpha^2 - \alpha) = 3$

from eqn. no. 26

$$I_{a1} = \frac{E_a}{Z_1 + Z_2 + Z_h} \quad \rightarrow 27$$

with fault impedance Z_h

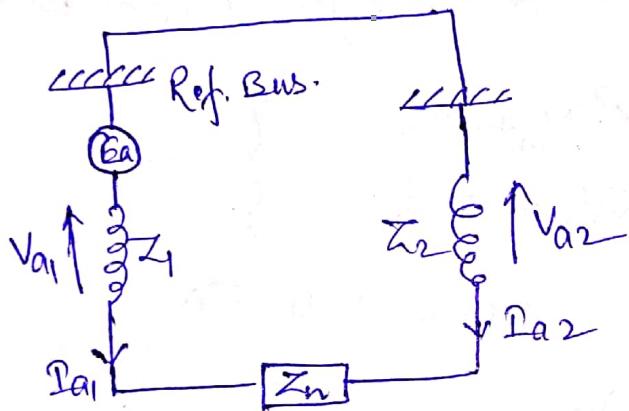
The phase currents are

$$\begin{bmatrix} I_a \\ I_b \\ I_c \end{bmatrix} = \begin{bmatrix} 1 & 1 & 1 \\ 1 & \alpha^2 & \alpha \\ 1 & \alpha & \alpha^2 \end{bmatrix} \begin{bmatrix} 0 \\ I_{a1} \\ -I_{a1} \end{bmatrix}$$

The fault current is

$$I_b^2 - I_c^2 = (\alpha^2 - \alpha) I_{a1}$$

$$I_b = -j\sqrt{3} I_{a1}, \quad \rightarrow 28$$



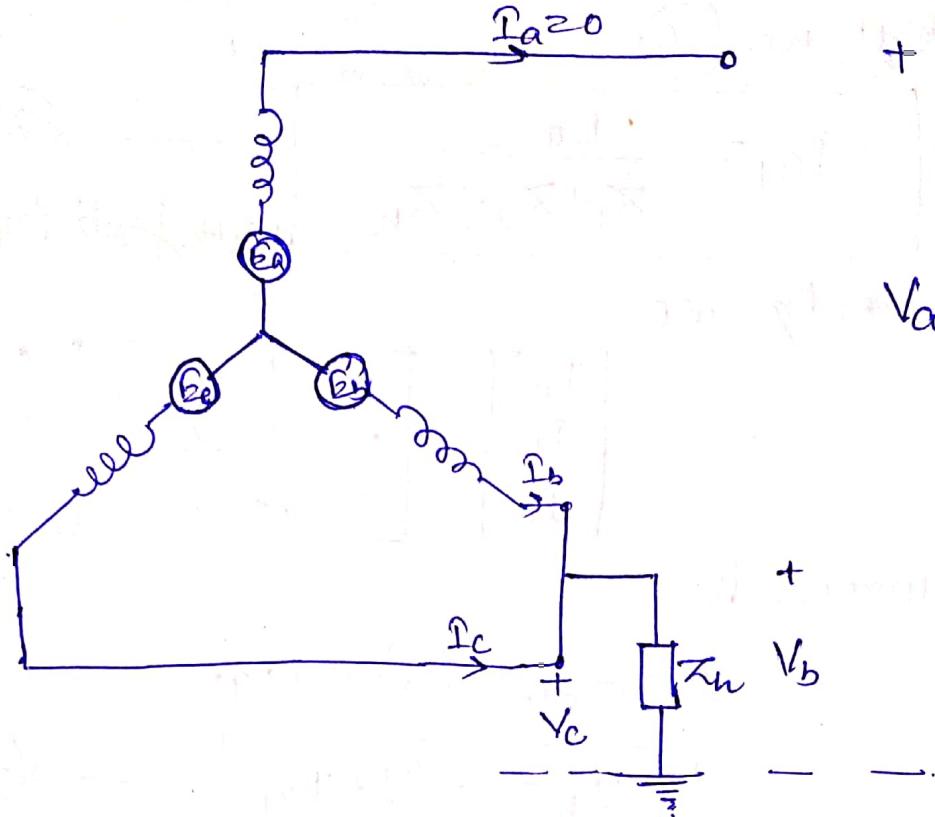
LLG Fault with fault impedance Z_h

Figure shows a 3-φ generator with a fault on phases 'b' and 'c' through an impedance Z_h to ground.

Assuming the generator is initially on no-load, the boundary conditions at the fault point are —

$$V_b = V_c = Z_f (I_b + I_c) \quad \rightarrow 29$$

$$I_a = I_{ao} + I_{a1} + I_{a2} = 0 \quad \rightarrow 30$$



Relationship b/w phase voltages & its symmetrical components

$$\begin{aligned} V_b &= V_{a0} + \alpha^2 V_{a1} + \alpha V_{a2} \\ V_c &= V_{a0} + \alpha V_{a1} + \alpha^2 V_{a2} \end{aligned} \quad \left. \right\} \rightarrow 31$$

since \$V_b = V_c\$, from above eqn. 31

$$V_{a1} = V_{a2} \quad \rightarrow 32$$

Put the symmetrical components of currents \$I_b\$ & \$I_c\$ in eqn. 29

$$\begin{aligned} V_b &= Z_h (I_a + \alpha^2 I_{a1} + \alpha I_{a2} + I_{a0} + \alpha I_{a1} + \alpha^2 I_{a2}) \\ &= Z_h (2I_{a0} - I_{a1} - I_{a2}) \quad \left. \right\} \{ 3I_{a0} - I_{a0} - I_{a1} - I_{a2} \} \\ V_b &= 3Z_h I_{a0} \quad \rightarrow 32 \end{aligned}$$

Put the value of \$V_b\$ & \$V_{a2}\$ from eqn. 33 & 32 in eqn. 31

$$3Z_h I_{a0} = V_{a0} + (\alpha^2 + \alpha) V_{a1}$$

$$3Z_n I_{ao} = V_{ao} - V_{a1} \rightarrow (32)$$

from eqn. (2)

$$3Z_n I_{ao} = -Z_0 I_{ao} - [E_a - Z_1 I_{a1}]$$

$$(3Z_n + Z_0) I_{ao} = -(E_a - Z_1 I_{a1})$$

$$I_{ao} = \frac{-(E_a - Z_1 I_{a1})}{Z_0 + 3Z_n}$$

→ (33)

Put the value of V_{a1} & V_{a2} in eqn. (32) from eqn. (2)

$$E_a - Z_1 I_{a1} = -Z_2 I_{a2}$$

$$I_{a2} = \frac{-(E_a - Z_1 I_{a1})}{Z_2}$$

→ (34)

Put the value of I_{ao} & I_{a2} from eqn. (33) & (34) in eqn. (30) & solve for I_{a1} —

$$I_{a1} = \frac{E_a}{Z_1 + \frac{Z_2(Z_0 + 3Z_n)}{Z_2 + Z_0 + 3Z_n}}$$

With fault impedance Z_n

Finally the fault current $I_f = I_b + I_c = 3I_{ao}$

