

## On-Load starting.

### (i) Damper Winding starting. (amortisseur)

- To make synchronous motor self-starting, damper windings are placed in rotor pole faces.
- Damper windings are made up of thick copper wires or copper bars.
- These damper windings are shorted at both the ends using metal rings.
- So, the arrangement of damper windings is similar to squirrel cage windings of a 3-phase induction motor.
- Initially, 3-phase ac supply is given to stator winding, which produces a rotating magnetic field.
- Rotor is not energised initially. So, the rotating magnetic field cuts damper windings, which act as squirrel cage. So, the motor starts rotating as squirrel cage induction motor.
- When the speed of rotor reaches near synchronous speed, the rotor is given DC supply.
- The rotor is pulled into synchronism and stator and rotor field gets magnetically interlocked, producing a stable unidirectional torque.

## Methods of starting synchronous motor

There are two methods of starting synchronous motor.

(i) DC field excitation (using DC supply)

DC field current is supplied to the field winding of the motor.

DC field current is proportional to the starting torque and hence it is proportional to the starting current.

It is a simple method but it is not economical because it requires large DC power source.

### (ii) Variable voltage and frequency starting (keeping $\frac{V}{f} = \text{constant}$ )

- With advances in power electronics, variable frequency supply can be easily obtained.

- This method is used to start the synchronous motor on no load.

- Initially, both voltage and frequency is kept low, keeping  $\frac{V}{f}$  ratio constant to avoid saturation of machine core.

- So, after giving low voltage and low frequency supply to the stator, rotor is given DC supply.

- Since, input frequency of stator supply is very low, so, rotating magnetic field also rotates slowly and rotor is able to catch up with this rotating magnetic field.

- Once stator and rotor fields are magnetically interlocked at low frequency, we can now increase voltage and

frequency to its rated ~~voltage~~<sup>value</sup>, keeping  $\frac{V}{f}$  constant.

## Armature Reaction in Synchronous Motors.

### In Synchronous generators

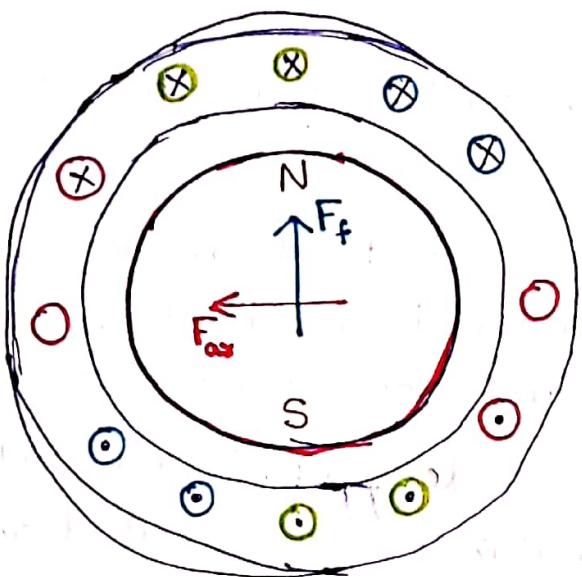
- When we talk about power factor, it is that of the alternator itself.
- When we are seeing the effect of armature reaction, we take the current to be Leading, Lagging or at unity p.f. and accordingly see if effect is magnetising or de-magnetising and accordingly whether alternator is over-excited or under-excited.
- But, in actual, we adjust the excitation of the machine first and accordingly the machine works on leading or lagging power factor.

### In synchronous motor

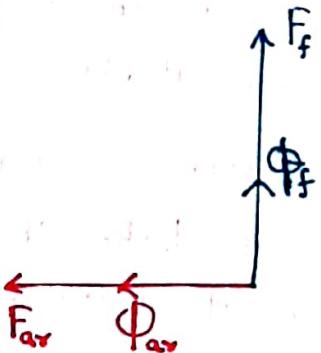
- Here also, the power factor we are talking about is that of the motor itself, i.e. whether motor is working on lagging or leading p.f.
- While analysing effect of A.R., we take current to be leading or lagging first and see if motor is under-excited or over-excited.
- But, in actual, we adjust the excitation of the motor first and accordingly see if machine is working on leading or lagging power factor.

## Armature Reaction in Synchronous Motor

### (i) Unity power factor

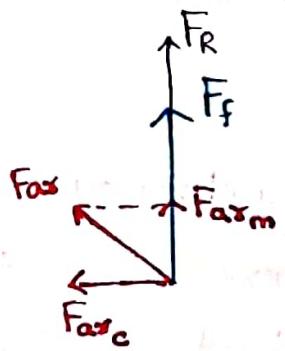
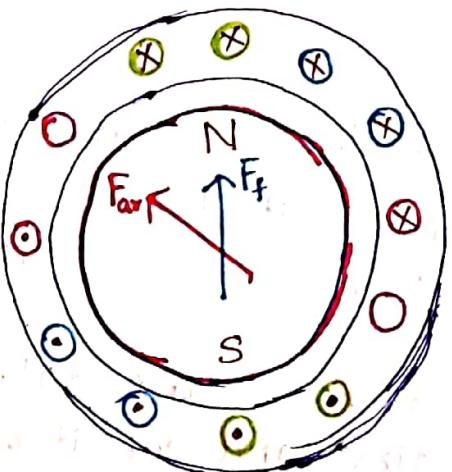


cylindrical rotor  
Synchronous motor  
at unity p.f.



$\therefore$  Effect of armature reaction  
at unity p.f. is cross-magnetising

### (ii) lagging p.f.

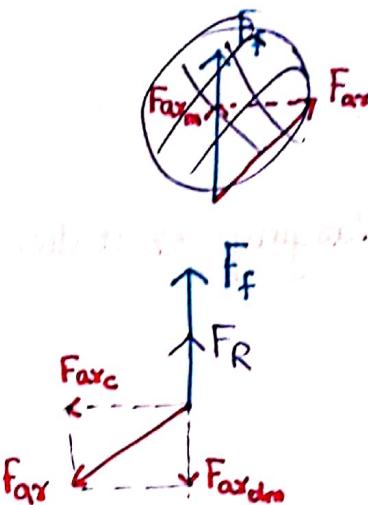
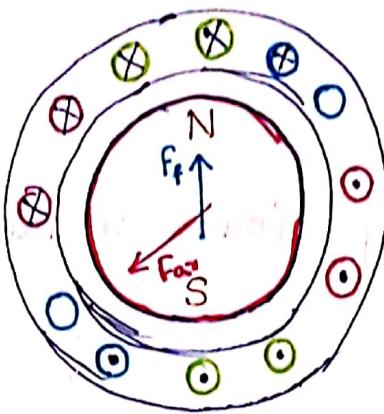


- So, at any lagging power factor,  
armature reaction is both  
magnetising and  
cross-magnetising.

- Motor is under-excited.

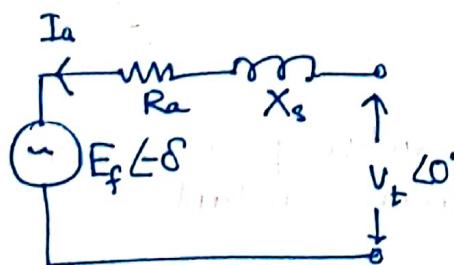
Underexcited condition is due to low voltage or high resistance in the armature winding.

### (iii) Leading p.f.

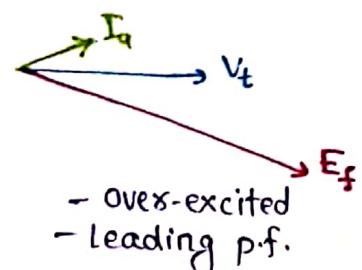
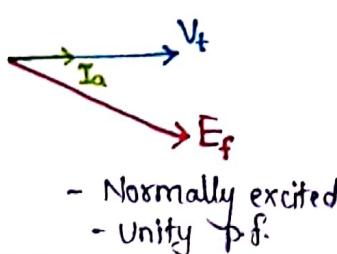
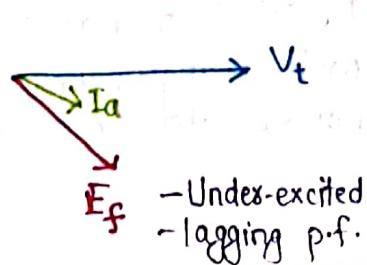


- So, effect of armature reaction is both cross-magnetising and de-magnetising.
- Motor is over-excited

### Equivalent circuit and phasor diagram.



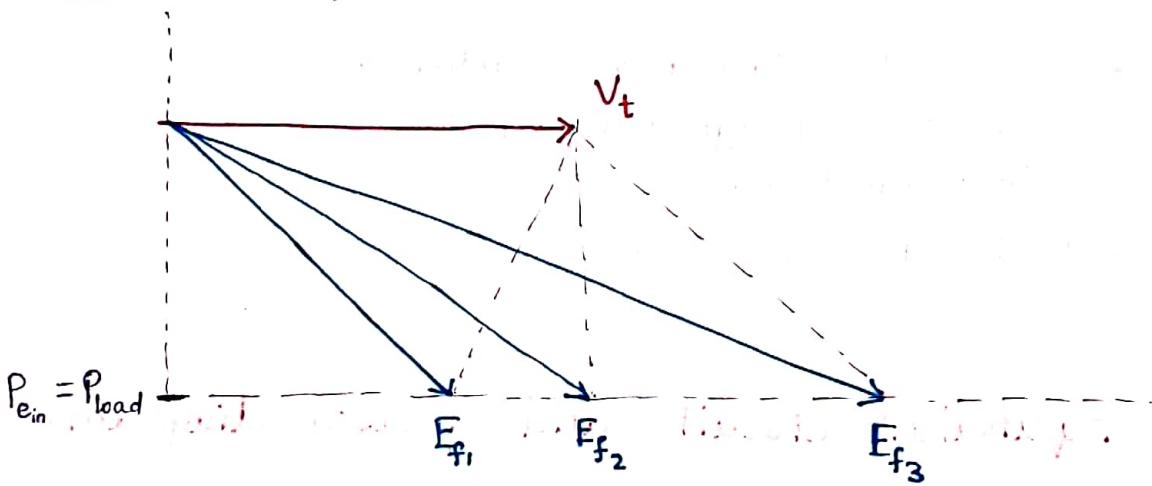
- Active power flows from Leading angle to lagging angle. So, if we keep  $V_t$  as reference, at  $0^\circ$ , then  $E_f$  will be at  $-\delta$ , for the machine to act as synchronous motor and consume active power.



# Effect of varying field current at different loads.

## ① Excitation curve.

(i) - Varying excitation keeping Load constant.



- Load is constant  $\Rightarrow$  So, active power consumed will remain constant
- With changing excitation  $\Rightarrow$  Only reactive power taken or delivered by motor changes.
  - $\Rightarrow$  Armature current  $I_a$  changes but that is because of changing reactive power.  $I_a \cos\phi$  remains constant with changing  $I_a$ , so active power taken remains constant.

$$P_{in} = \frac{V_t \cdot E_f}{X_s} \sin \delta$$

$V_t$  = Constant

$X_s$  = Constant

$P_{in}$  = Constant.

$\therefore E_f \sin \delta = \text{Constant.}$

→ So, with change in excitation, but load remaining constant,  $E_f \sin \delta$  remains constant.

→ Only  $E \cos \delta$  changes, depending on which the reactive power taken or delivered by the synchronous motor changes.

Similarly,

$$P_{in} = V_t \cdot I_a \cos \phi$$

$P_{in} \rightarrow \text{constant}$

$V_t \rightarrow \text{constant.}$

So,  ~~$I_a$~~   $I_a \cos \phi = \text{constant.}$

keeping load constant,

→ So, with changing excitation,  $I_a$  changes, but  $I_a \cos \phi$  remains constant.

→  $I_a$  changes to meet the reactive power requirement.